

Convective atmospheric boundary layer using Large Eddy Simulation

U. Vigny^{a,b}, L. Voivenel^b, S. Zeoli^a, P. Benard^b

^a Université de Mons (UMONS), Polytechnic Faculty, Belgium

^b CORIA, CNRS UMR6614, Normandie Université, INSA and University of Rouen, France

18th EAWE PhD Seminar - 2022

Theme: Wind farms and wakes

Context: Global warming

Context

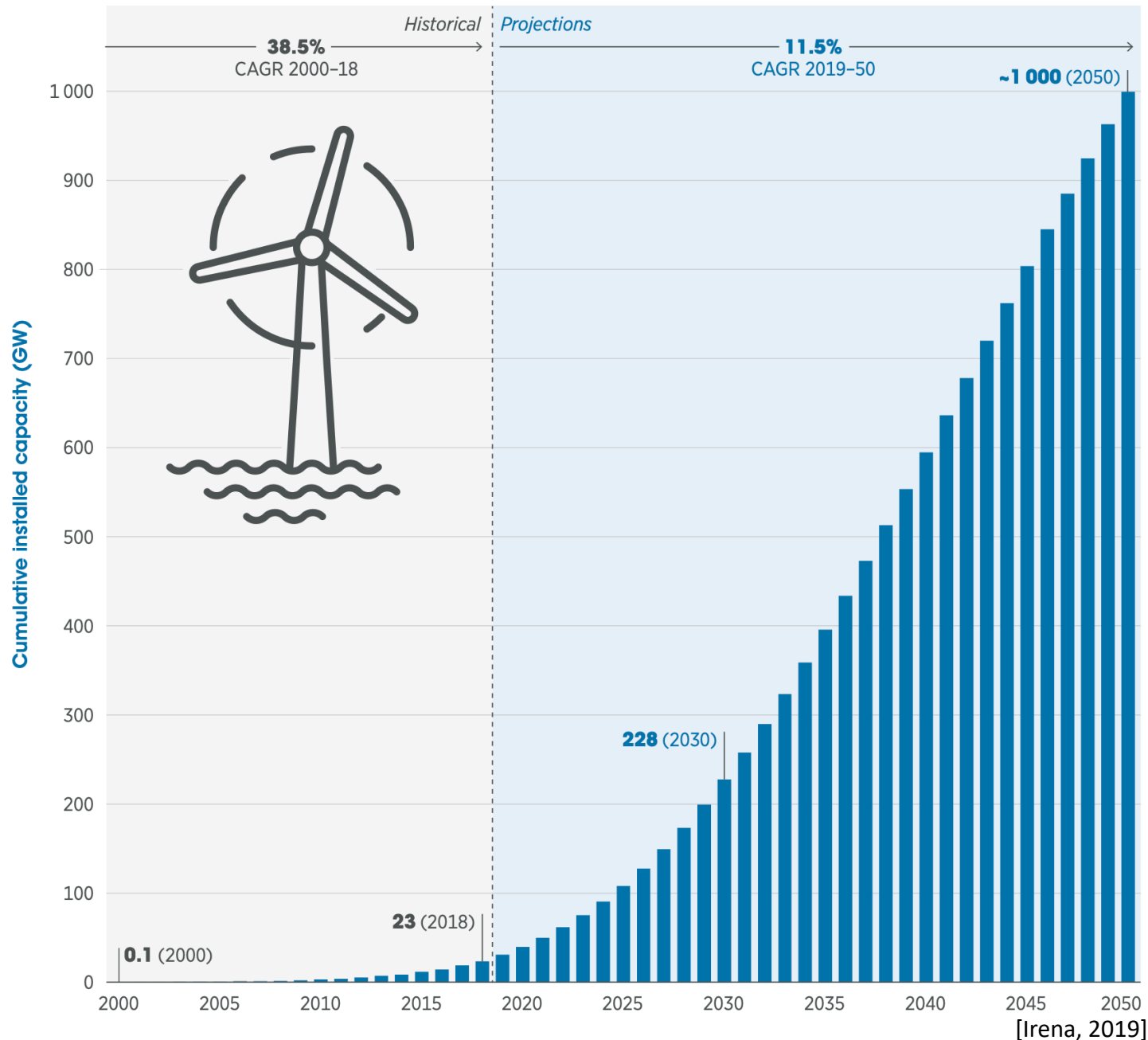
- Carbon neutral 2050
 - Reduce CO₂ emissions
 - Shift energy production

Wind energy

- Potential
 - 30 – 39 PWh /year potential in Europe
- Competitiveness
 - competitive LCOE
 - Carbon footprint
- Prevision
 - X10 in 30 years

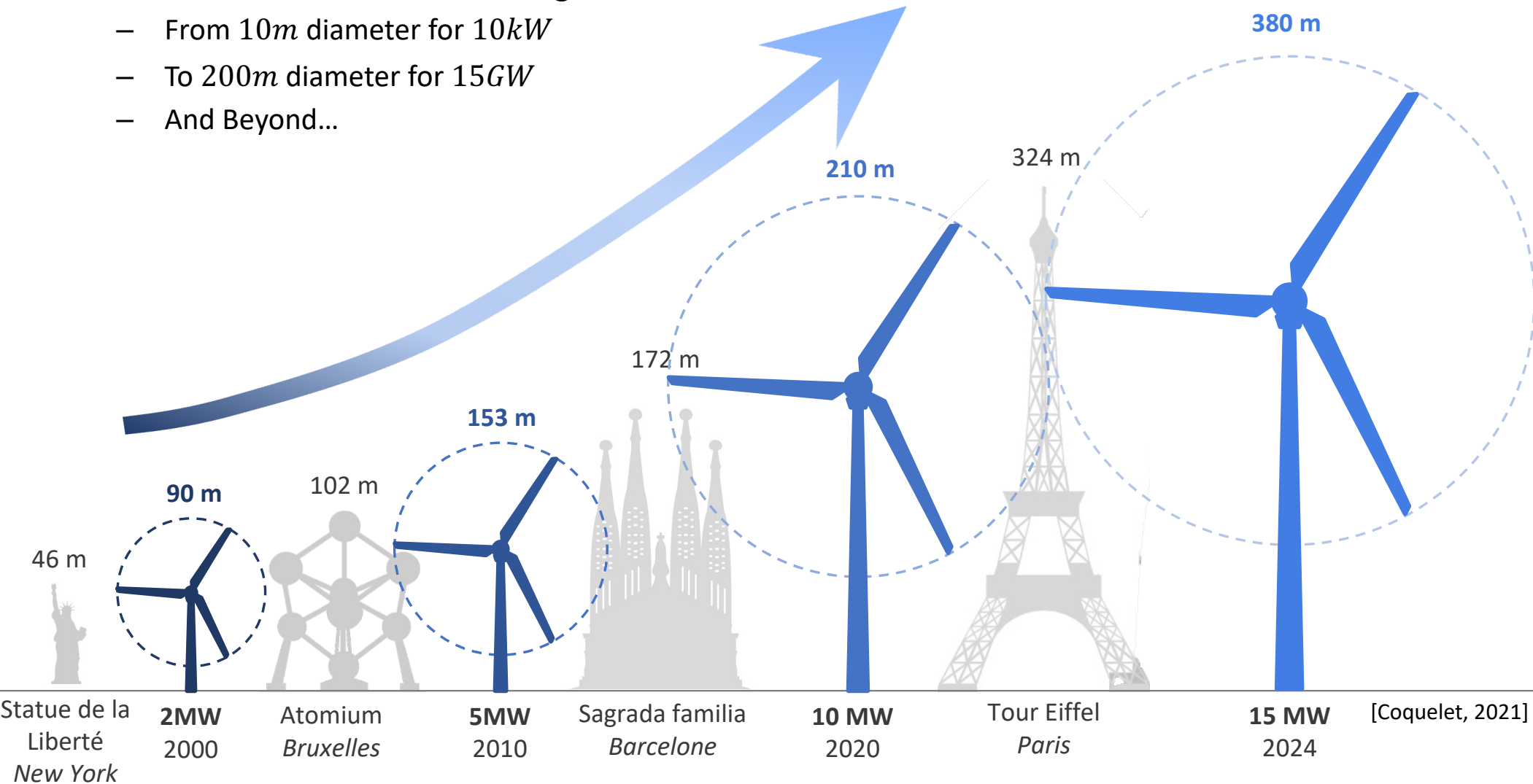
Power production

- Strong and regular wind
- Efficiency
- Wind turbine size



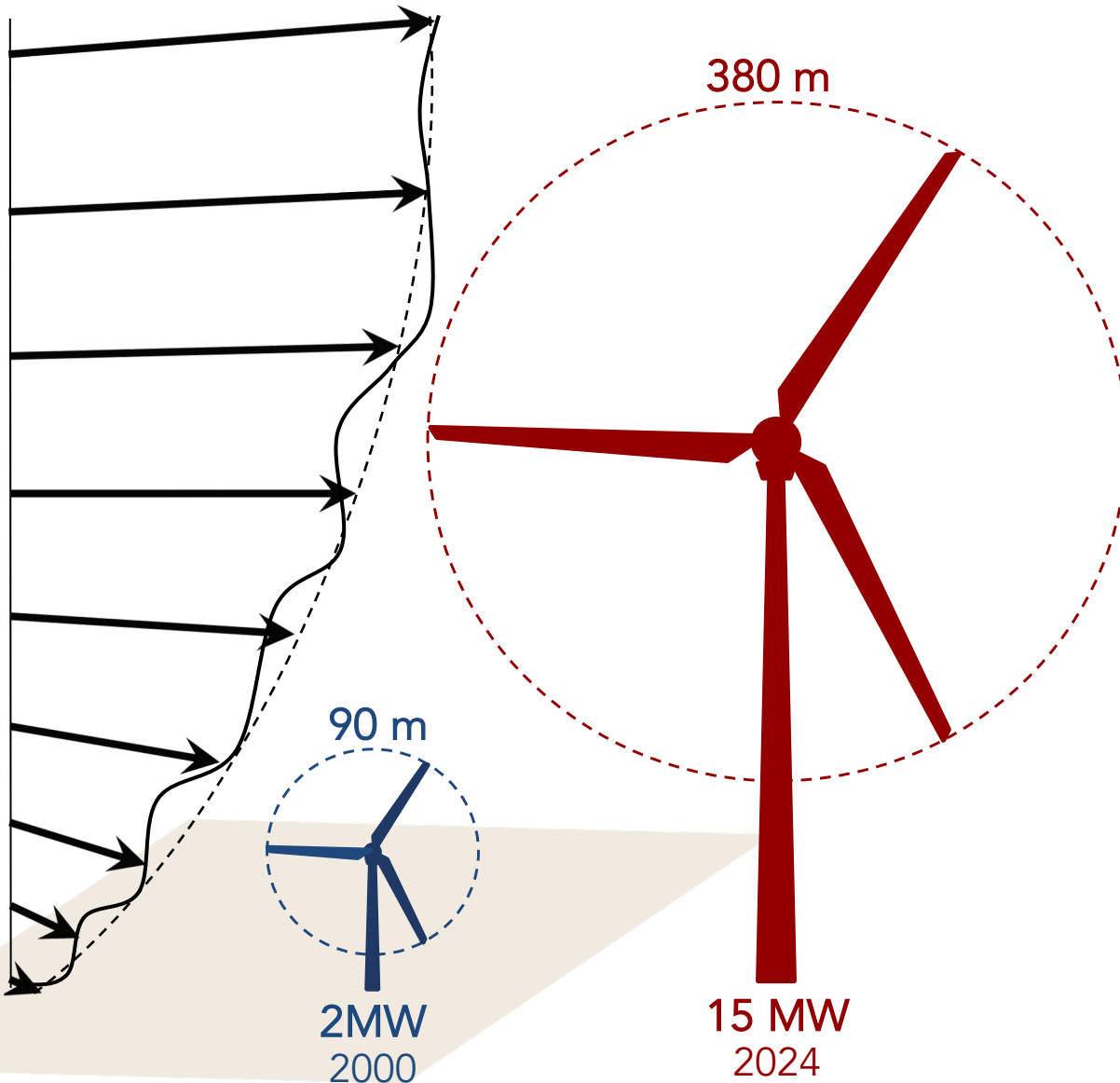
Wind turbine modelling

- Offshore rotor size continues to grow
 - From 10m diameter for 10kW
 - To 200m diameter for 15GW
 - And Beyond...



→ Different flow physics

Microscale to Mesoscale



Weather study

Meso-scale

- Free atmosphere $\sim O[10km]$
 - Constant temperature gradient
 - Non-turbulent
- Inversion layer $\sim O[100m]$
 - Discontinuity in temp & velocity
 - Strong thermal stability
 - Rigid lid on top of the ABL
- Mixed layer $\sim O[500m]$
 - Neutral, stable, convective ABL
 - Turbulent layer

Small scale study

Micro-scale

- Inertial sublayer $\sim O[50m]$
 - Bulk exchange of mass, momentum and heat (wind-waves)
- Wave boundary layer $\sim O[1m]$
 - Impacted by the motion of the waves
- Viscous sublayer $\sim O[1mm]$
 - Important viscous fluid forces

→ Mixed layer impact on wind turbines

The Mixed layer

Why the study

- Wind turbine wakes
 - Recovery, size
 - velocity deficit, turbulence
- Wind turbine aerodynamics
 - Power production, loads, fatigues

Why a challenge

- Thermal effect
 - Neutral, Stable, Convective

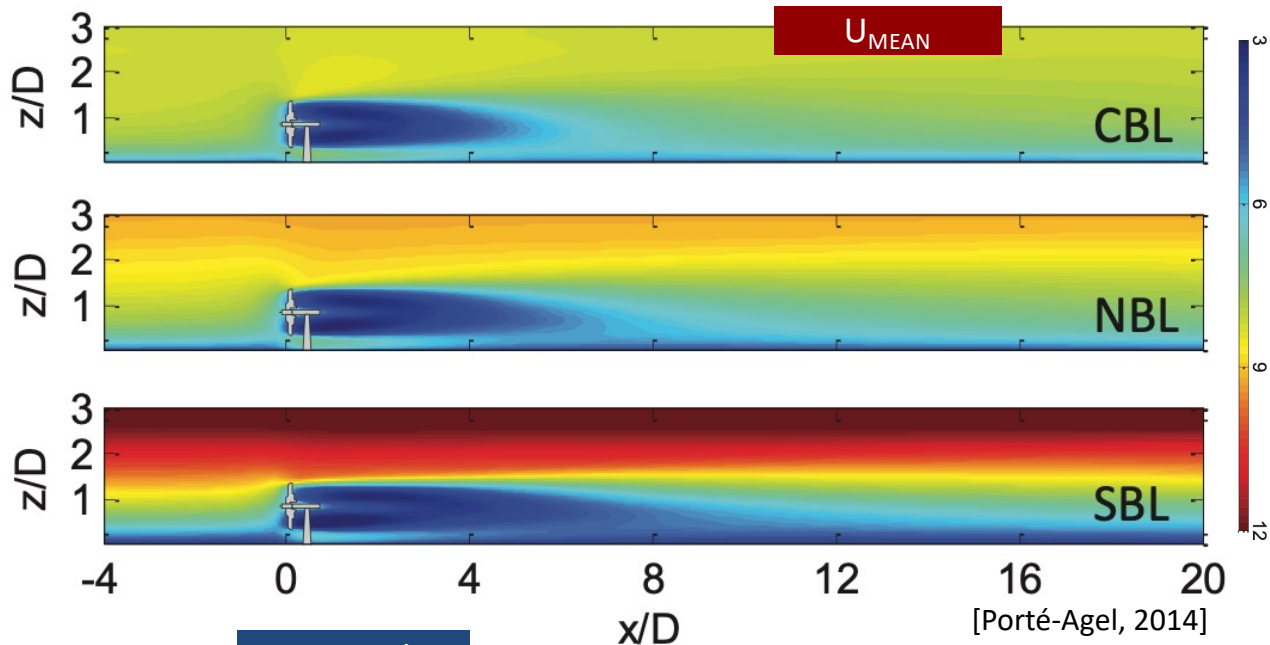
How to Model

- Monin-Obukhov similarity theory¹

$$\frac{u(z)}{u_\tau} = \frac{1}{\kappa} \left[\ln \left(\frac{z + z_0}{z_0} \right) - \Psi_m \left(\frac{z}{L} \right) \right]$$

$$\frac{\theta(z) - \theta_w}{\theta_*} = \frac{1}{\kappa} \left[\ln \left(\frac{z + z_0}{z_0} \right) - \Psi_h \left(\frac{z}{L} \right) \right]$$

$$\Psi_{m/h} = \int_0^{z/L} \frac{1 - \phi_{m/h}}{\xi} d\xi$$



$$\begin{cases} \phi_m(z/L) = 0 \\ \phi_h(z/L) = 0 \end{cases}$$

Neutral

$$\begin{cases} \phi_m(z/L) = 1 + \gamma_m \frac{z}{L} \\ \phi_h(z/L) = 1 + \gamma_h \frac{z}{L} \end{cases}$$

Stable

$$\begin{cases} \phi_m(z/L) = \left(1 - \beta_m \frac{z}{L} \right)^{-1/4} \\ \phi_h(z/L) = \left(1 - \beta_h \frac{z}{L} \right)^{-1/2} \end{cases}$$

Convective

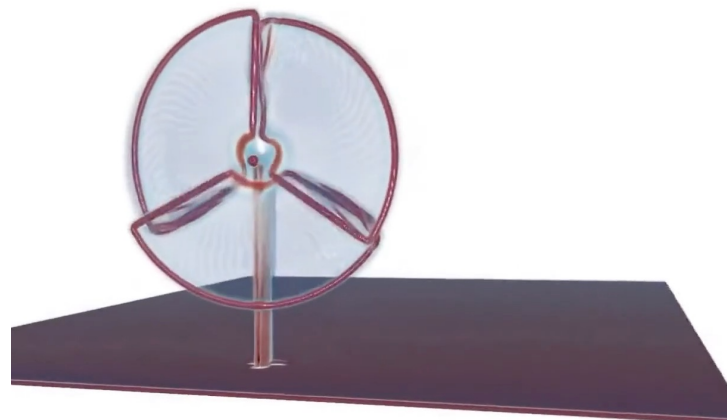
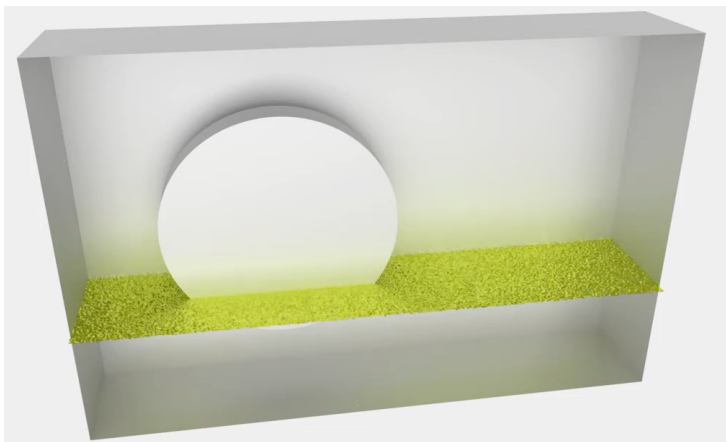
- Obukhov length: $L = -\frac{u_\tau^3 \theta_0}{\kappa g q_w}$
- Friction velocity: u_τ
- Roughness length: z_0
- Von Karman $\kappa = 0.37 \sim 0.41$
- Wall temperature: θ_w
- Heat flux: $q_w = \theta_* \times u_\tau$

- Long term goal → Accurate analyse of the interaction between wind turbines and ABL
- Presently → Convective ABL simulation

- Large Eddy Simulation → Large scale resolution, small scale modelling

YALES2 features

- **Unstructured meshes** and adaptive grid refinement
- **Low-Mach number** Navier-Stokes equations (incompressible and **variable density**) solved with projection method
- Double domain decomposition¹
- Highly efficient solvers for linear system inversion (PCG, DPCG)²
- **4th order** central finite volume method and **4th order** time integration³
- Suited for **massively parallel computing** (>32 000 procs)
- Actuator Line Method⁴



Application to a dry convective boundary layer

Willis & Deardorff test case:

- Periodic box
 - Uniformly heated $q_w = 0.06 \text{ Kms}^{-1}$
 - Initial temperature $\theta_0 = 299.7 \text{ K}$
 - Initial height $z_m = 1350 \text{ m}$
- Inversion layer
 - $\frac{d\langle\theta\rangle}{dz} = 0.003 \text{ K}\cdot\text{m}^{-1}$
- Random perturbation
 - $r \in [-0.5; 0.5]$

Initial velocity profile

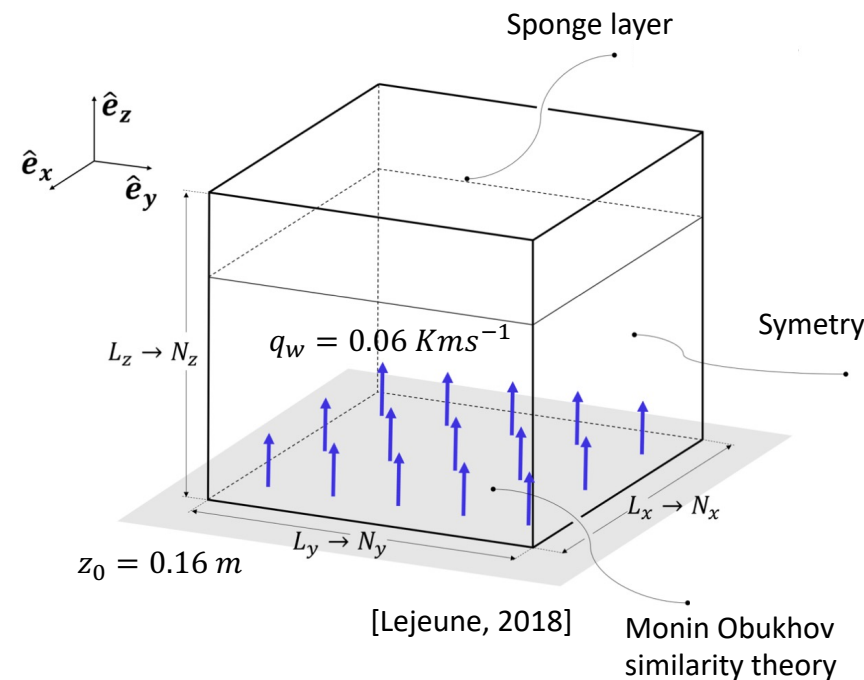
$$w(z) = \begin{cases} 0.1r \left(1 - \frac{z}{z_m}\right) w_c^0, & \text{if } 0 < z \leq z_m \\ 0, & \text{if } z > z_m \end{cases}$$

Initial temperature profile

$$\theta(z) = \begin{cases} \theta_0 + 0.1r \left(1 - \frac{z}{z_m}\right) \theta_c^0, & \text{if } 0 < z \leq z_m \\ \theta_0 + (z - z_m) \frac{d\langle\theta\rangle}{dz}, & \text{if } z > z_m \end{cases}$$

3 comparison studies

- J.G. E. Willis & J. W. Deardorff 1974 → 1st experimental setup
- J. W. Deardorff & G. E. Willis 1985 → Further results
- H. Schmidt & U. Schumann 1988 → LES

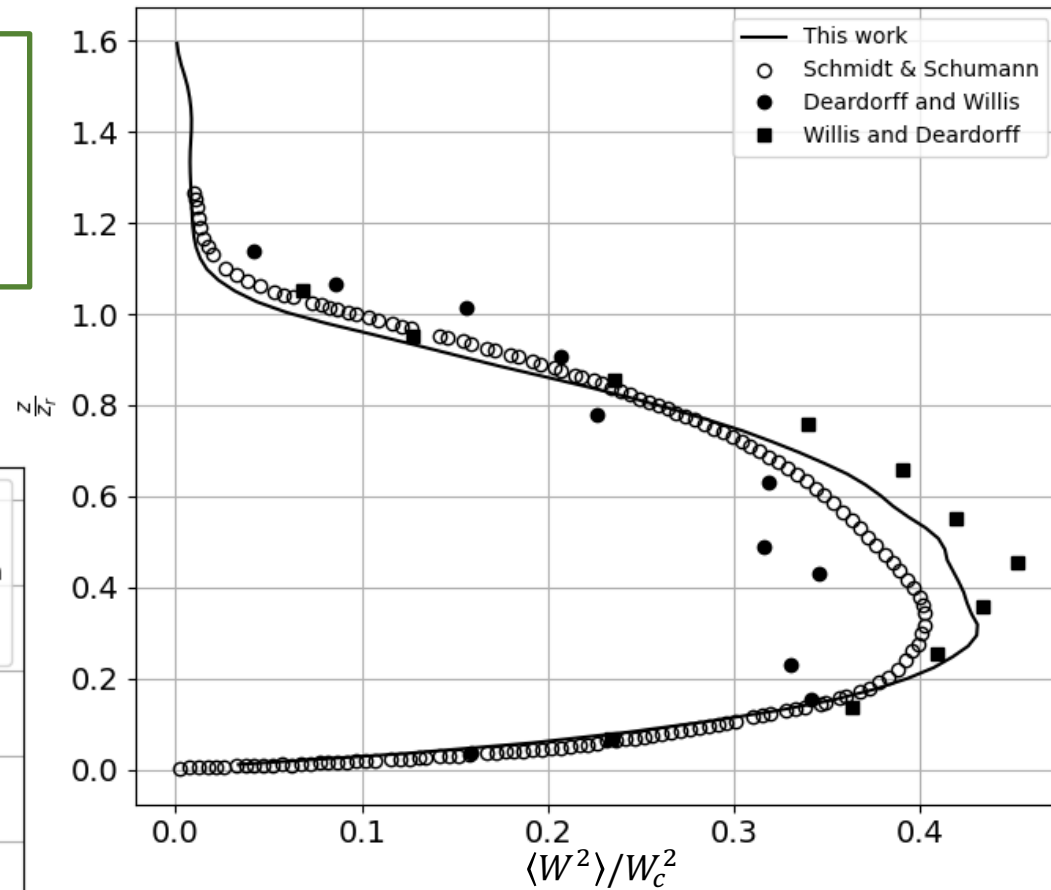
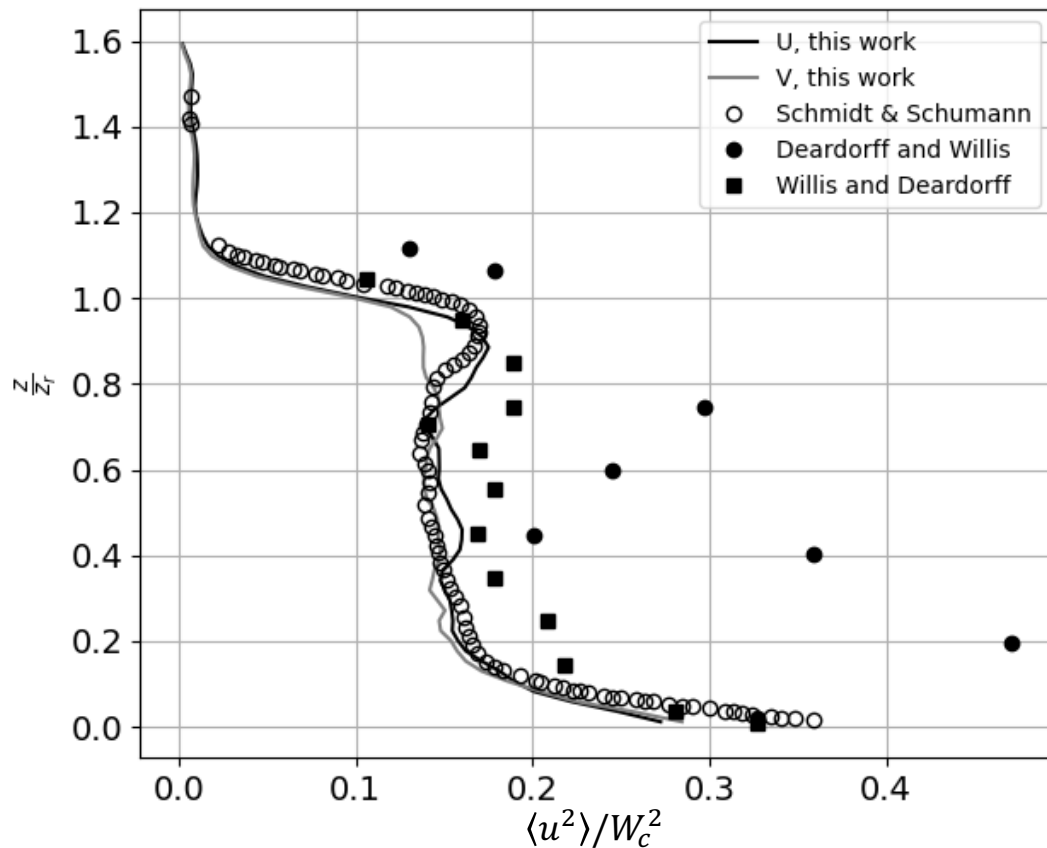


Case	W&D	S&S	This work
Top BC	insulate	Radiation	Sponge Layer
Lateral BC	wall	Symetry	
Lower BC	heat exchanger	Monin-Obukhov similarity theory	
SGS Model	/	TKE Based	Smagorinsky
Initial contidions	/	Mixed layer topped by fluctuations	
Comp. domain	water	160×160×48	256×256×128
Physical domain	114×122×76 cm	8000 × 8000 × 2400 m ³	

Horizontal & vertical velocity variance

- Matches Schmidt & Schumann numerical results
- Deardorff & Willis: higher horizontal velocity variances

→ Due to surface heat flux horizontal variation



- Vertical → buoyancy (larger overall)
- Horizontal → pressure fluctuations (predominant at the mixed layer edges)

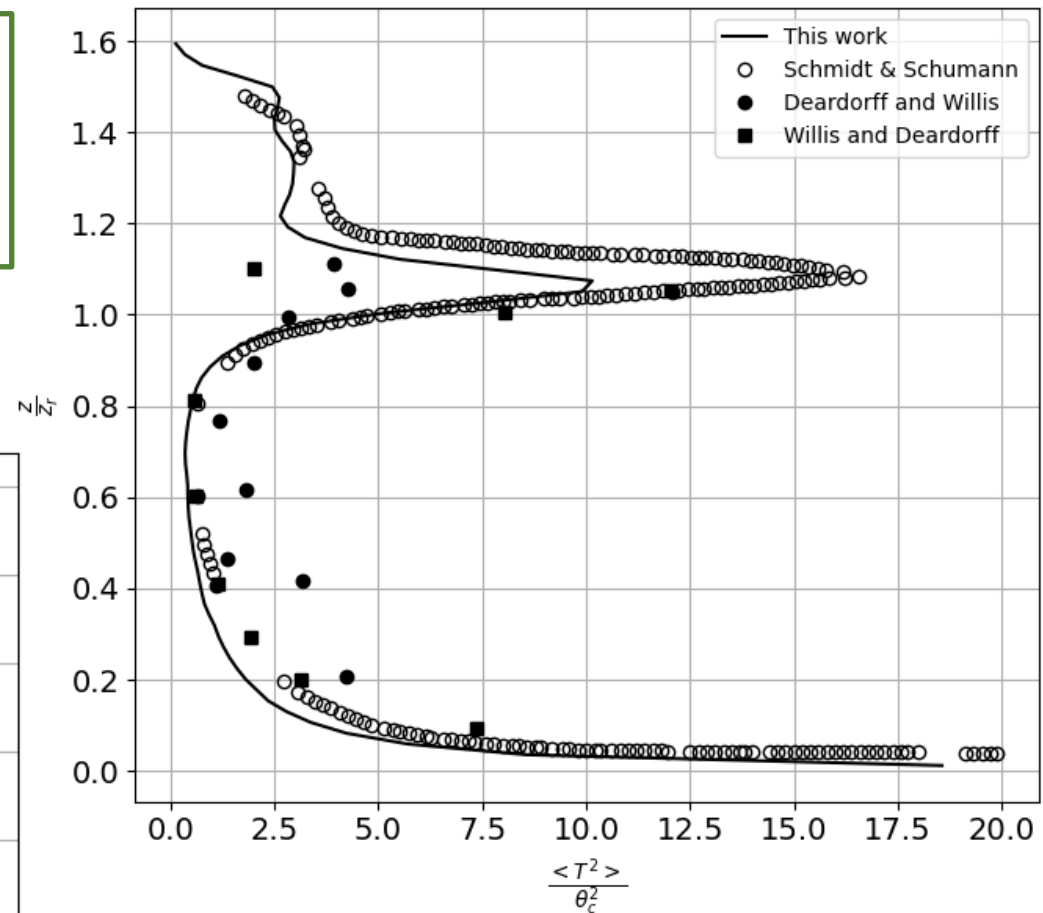
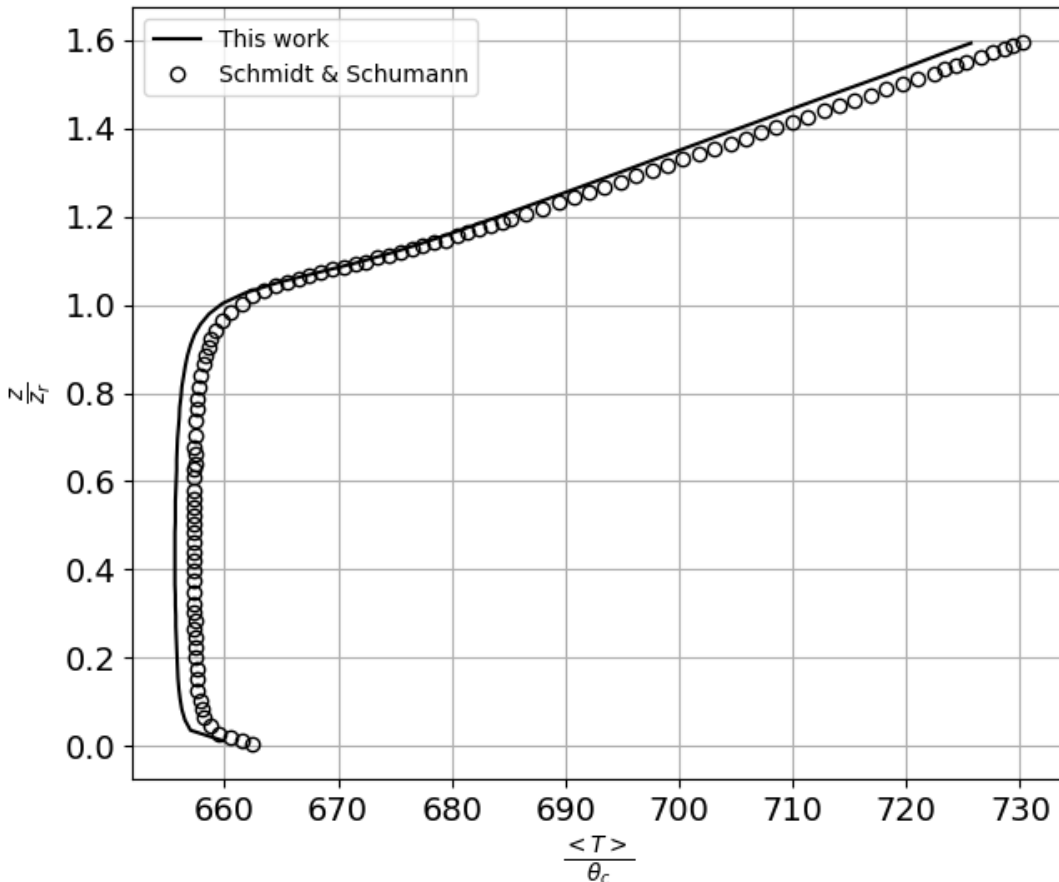
→ Overall lower horizontal than vertical velocity variance

Mean temperature & temperature variance

Mean Temperature

- Constant temperature in the mixed layer (intense turbulent mixing)
- Quasi-steady state reached

→ Matches numerical results



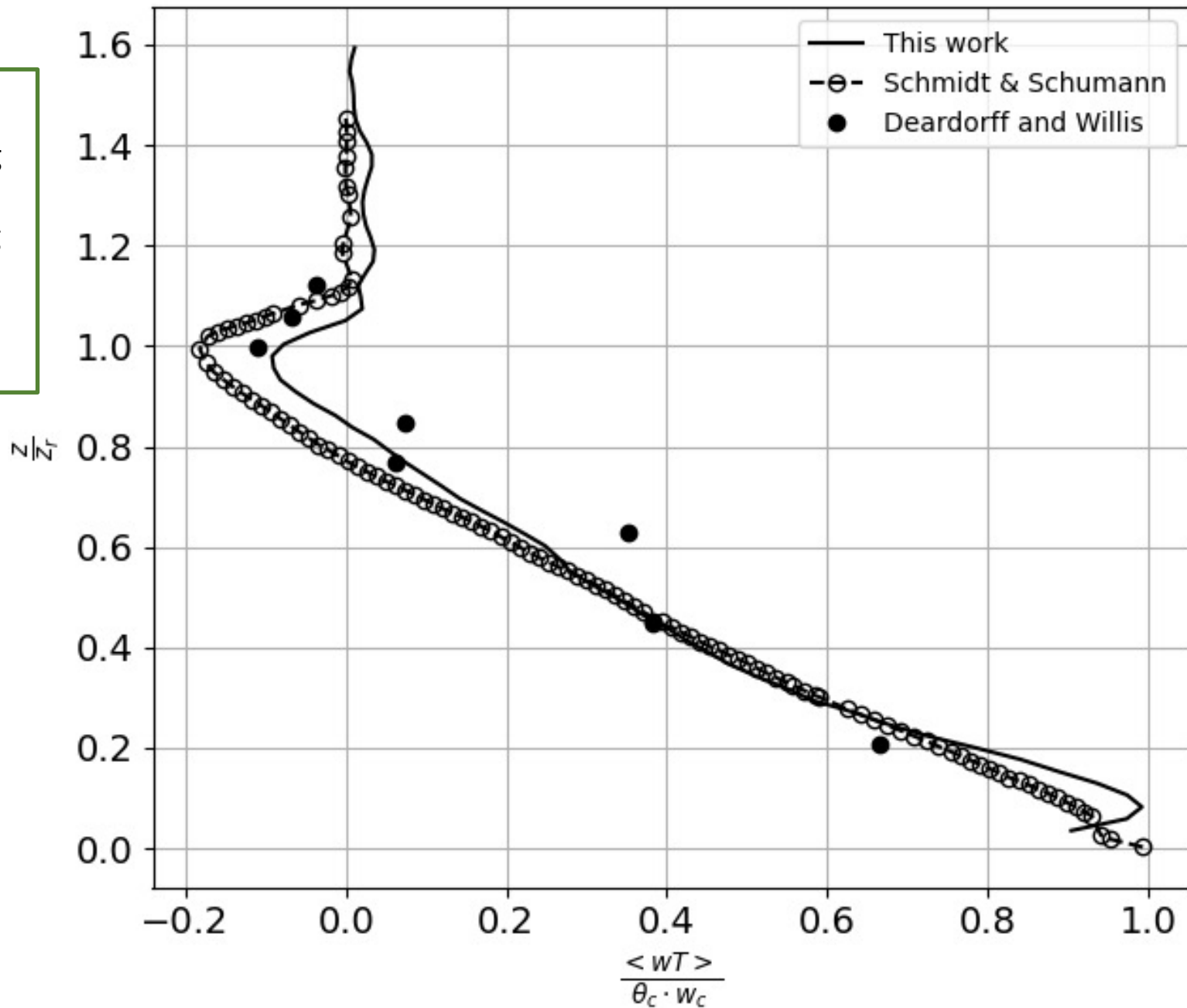
Temperature variance

- Heat flux and temperature gradient product
- Low overall
- High at the mixed layer edges

→ Matches both experimental & numerical results

Vertical heat flux

- Trends as expected
 - Linear decreasing with height (constant heating rate)
 - Stable at the inversion layer



→ Matches both experimental & numerical results

Conclusion and further work

Conclusion

- Implementation of the Monin-Obukhov similarity theory into YALES2
- Application on a literature test case
- Validation with experimental and numerical literature results

Perspectives

- Convective boundary layer wind farm simulation
- Stable boundary layer consideration

UMONS
Université de Mons

coRia
UMR 6614

