

A first step to study numerically the tool wear influence in Ti6Al4V orthogonal cutting

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Context

Aeronautical industry : part reliability = important requirement

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◆ Part reliability ➡ surface integrity should be mastered = still a challenge in machining up to now

Experimental challenges	Numerical challenges
◆ Influence of tool wear on microstructure and surface integrity (SI) [1], evolution of tool geometry with the increase of wear ➡ difficult ongoing problem	From a numerical point of view, challenges : prediction of residual stresses [2], influence of tool geometry on residual stresses (RS) [3], prediction of tool geometry which evolves with
When should the tool be replaced? Not damaging the surface but using it until its end of life	the increase of wear [4, 5] + Current finite element models with updating tool geometry are rather heavy to compute

For Inconel 718 [6], experimental study shows the link between tool wear, cutting forces and machined surface ron numerical equivalent so far row first numerical step : influence of tool wear in Ti6Al4V machining with a non-adaptive tool geometry and a classical material constitutive law (Johnson-Cook)

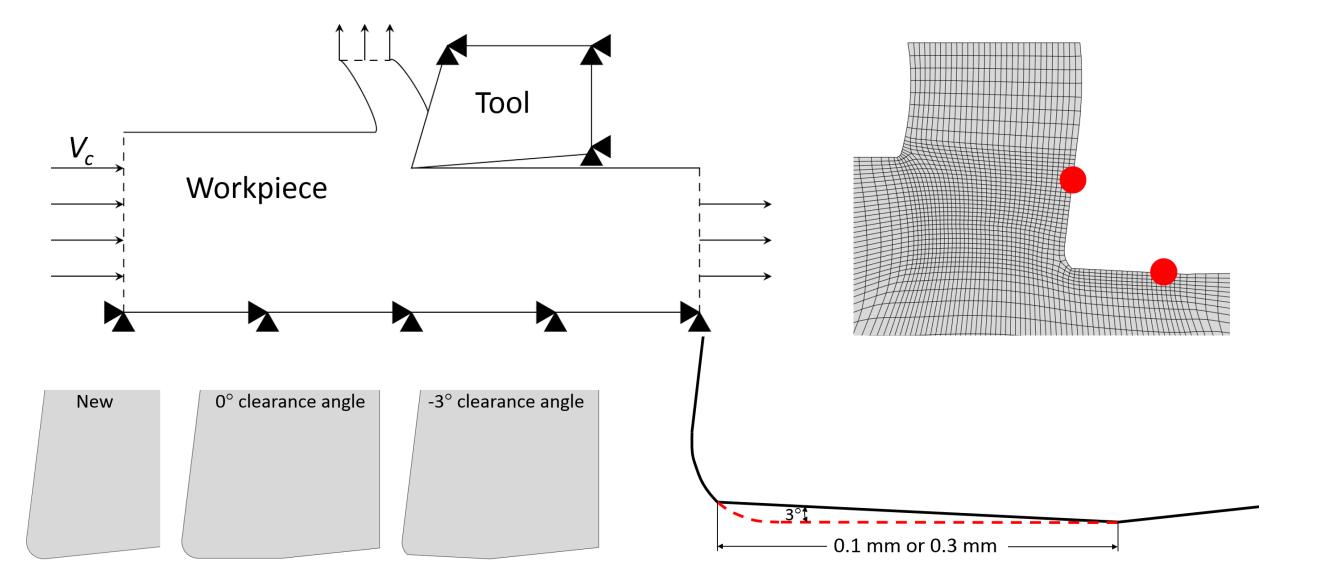
Finite element model

General features

- ◆ 2D plane strain orthogonal cutting model, Abaqus/Explicit v6.11
- + Arbitrary Lagrangian Eulerian (ALE) formulation with Lagrangian and Eulerian boundary conditions
- Chip formation = adaptive meshing and plastic flow of material
- ◆ Refined meshes close to the cutting edge radius and shear zones (SZ)
- ◆ Typical industrial cutting speed : 80 m/min, uncut chip thickness : 0.1 mm

Tool geometries

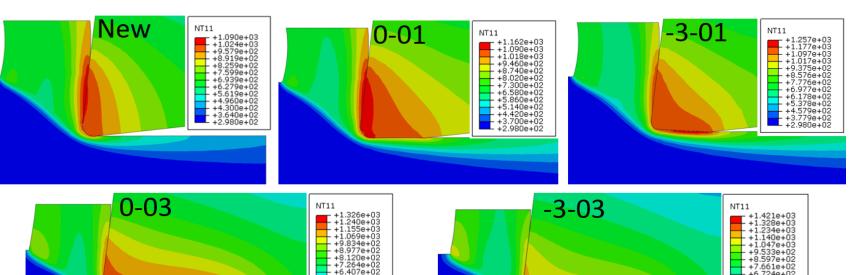
- ◆ 3 types of tool geometry to take tool wear into account, 5 geometries in total
- Fresh tool = rake angle : 7°, clearance angle : 6°, cutting edge radius : 20 μm

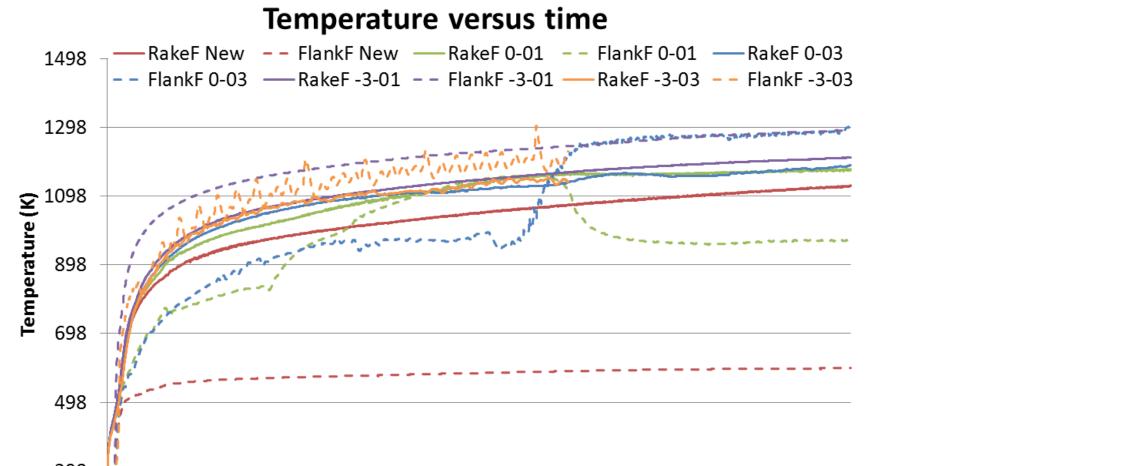


Results

Temperatures

- The location of the maximum temperature moves with tool geometry from SSZ to TSZ
- ✦ Increase of the temperature with tool wear



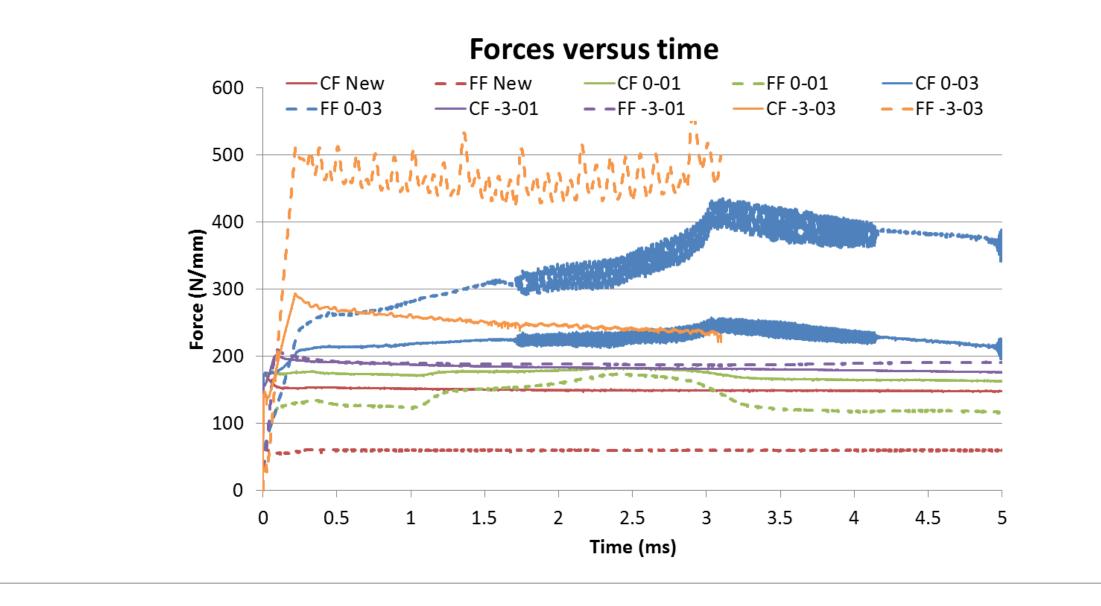






Cutting forces

- ◆ Tool wear ➡ increase of friction on clearance face ➡ forces increase with tool wear and particularly feed force
- ✦ Forces evolution ➡ chip are not continuous anymore
- ♦ 2 distinct evolutions depending on the clearance angle

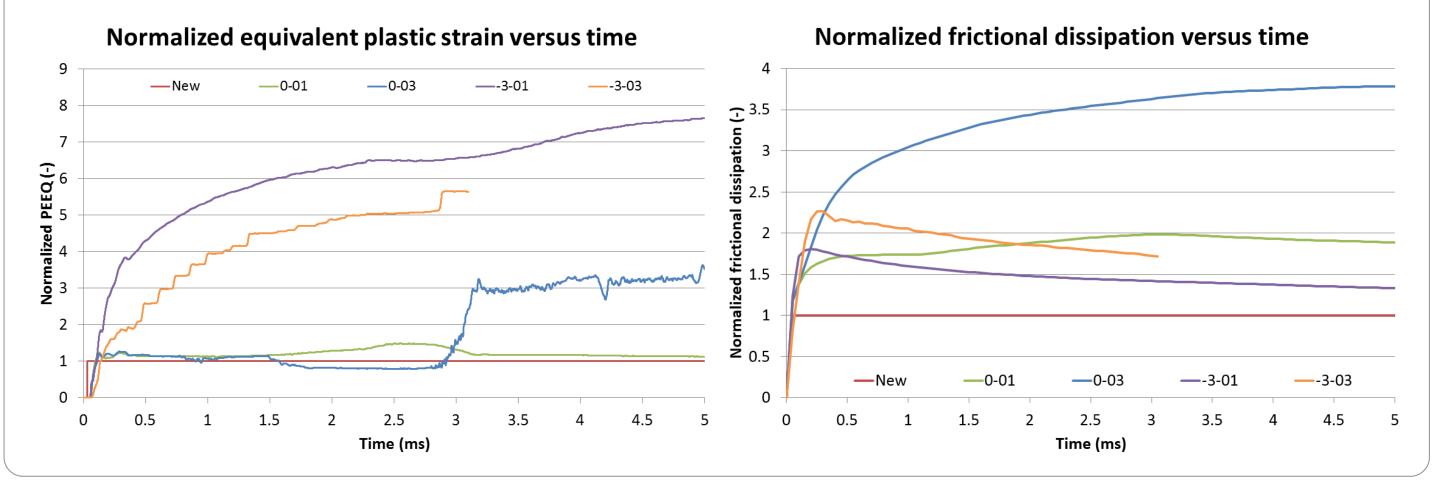


Plastic strains

- ♦ Normalized value = $\frac{\text{value with current tool geometry}}{\text{value with initial tool geometry}}$
- ✦ Higher equivalent plastic strain ➡ higher RS ➡ decrease in the quality of the part

Friction

- Frictional dissipation higher with wear, when clearance angle is 0° and when flank wear is larger
- ♦ 2 distinct evolutions depending on the clearance angle



References

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Conclusions and perspectives

♦ Tool wear influences the chip formation notably

 \diamond The most worn tool impacts the most the machined surface and the chip formation

The chip morphology is influenced by the tool geometry

♦ Measuring the cutting forces should help to detect experimentally a too much worn tool

♦ All the results were qualitatively in accordance with the literature

An experimental campaign in the same cutting conditions is planned to validate the numerical predictions

Improvements of the model will include an adaptive tool geometry and a constitutive law taking the microstructure modifications into account

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